IN THE SPECIFICATION:

Please amend the Specification as follows.

Page 4, paragraph beginning on line 17:

A bearing support assembly 4 is connected to the other axial end surface of the permanent magnet 2. This provides a highly compact structure. The turbine 3 may be made of ceramic material such as silicon nitride and silicon ~~carbine~~ carbide or heat resistance metallic material such as Inconel (Ni-based Ni-Cr-Fe alloy).

Page 5, paragraph beginning on line 6:

The bonding consisting of ~~sliver~~ silver brazing is carried out abutting a disk (having a thickness of 50 μm) made of the silver brazing material to a corresponding end surface of the shaft 3a of the turbine 3, and a disk (having a thickness of 500 μm) made of Koval on the outer end surface of the ~~sliver~~ silver brazing material. The end surface of the shaft 3a may have a surface roughness in the range of 0.8s to 3.2s, and the end surfaces of the Koval disk may have a surface roughness in the range of 3.2s to 25s.

Page 5, paragraph beginning on line 12:

The assembly was then heated in vacuum environment (1×10^{-4} to 1×10^{-6} torr or 1.33×10^{-2} to 1.33×10^{-3} Pa) from the room temperature to a maintaining temperature of 680 °C at the rate of 10 °C per minute, maintaining the temperature at 680 °C for one hour, and letting the brazing material cool naturally. During this heating process, the assembly was subjected to a bonding load of 0.1 ~~Mpa~~ MPa to 0.5 ~~Mpa~~ MPa. As a result

of this heating process, the thickness of the silver brazing material 6 was reduced to approximately 15 μm, and demonstrated some segregation.

Page 6, paragraph beginning on line 6:

The assembly was then heated in vacuum environment (1×10^{-4} to 1×10^{-6} torr or 1.33×10^{-2} to 1.33×10^{-3} Pa) from the room temperature to a maintaining temperature of 390 °C at the rate of 5 °C per minute, maintaining the temperature at 390 °C for one hour, and letting the brazing material cool naturally. During this heating process, the assembly was subjected to a bonding load of 0.1 ~~Mpa~~ MPa to 0.5 ~~Mpa~~ MPa. As a result of this heating process, the thickness of the neodymium brazing material 7 was reduced to approximately 33 μm.

Page 9, paragraph beginning on line 22 and bridging pages 9 and 10:

According to the foregoing embodiment of the present invention, because the shaft is not required to be passed through the rotor, an adequate volume for the permanent magnet that is required to provide an adequate amount of magnetic flux can be ensured without increasing the axial dimension. Furthermore, because the power transmitting shaft and permanent magnet are integrally joined to each other by brazing, and the bonded part and permanent magnet are protected from the centrifugal stress by the sleeve, the permanent magnet rotor having a drive source or load source integrally attached thereto can be designed as a highly compact unit. If the sleeve is made of ~~fiber-reinforce~~

fiber-reinforced plastic material which is electrically non-conductive, the eddy current loss can be avoided.